One-layer robust MPC: a multi-model approach

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Outline

Introduction Motivation

Multi-model description of the plant Basic Assumptions

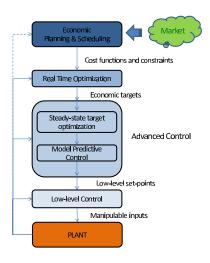
Multi-model one-layer MPC

Proposed formulation Properties

Example Simulation results

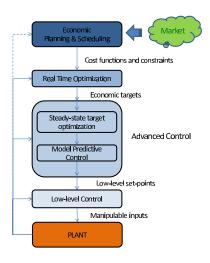
Concluding remarks Summary

Hierarchical control structure (Qin & Badgwell (2003); Engell (2007)):



- The Real Time Optimizer (RTO) computes the operation point according to economic criteria and operation limits.
- 2. The RTO solves an optimization problem based on a complex nonlinear stationary model of the plant.
- 3. The setpoints computed by the RTO are sent to the MPC control.
- MPC solves a QP based on a simplified dynamic model of the plant and constraints.

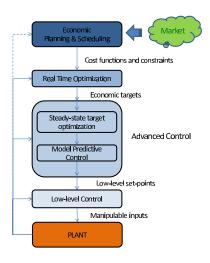
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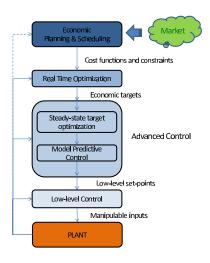
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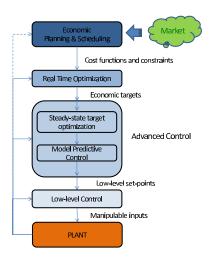
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- RTO time scale (hours or days) VS MPC time scale (minutes).
- Slow reaction to process variations (disturbances).
- There exist mismatches between the models of RTO and MPC.
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- SSTO or LP/QP-MPC (Muske (1997); Ying & Joseph (1999); Marchetti et al. (2014))
 - Same model as the MPC.
 - Same sample time as the MPC.
- One-layer solutions
 - Dynamic RTO (Biegler (2009); Kadam & Marquardt (2007); Würth et al. (2009))
 - One layer RTO+MPC (Adetola & Guay (2010); Zanin et al. (2002))
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- Plants has sparse operation points with different economics behaviors.
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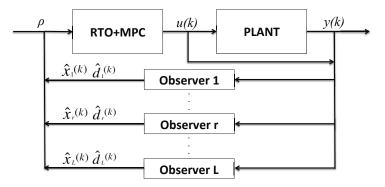
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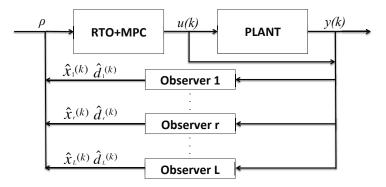


The real model of the plant is not known.

• We have a collection of linear model $\Pi = \{\pi_1, ..., \pi_L\}$ s.t.

 $\pi_i: \quad x_i^+ = A_i x + B_i u, \quad y_i = C_i x, \quad i \in \mathbb{I}_{1:L}$

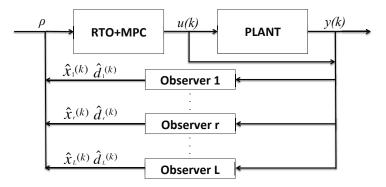
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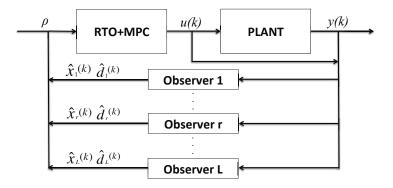
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Define an augmented system with an integrating output disturbance:

$$\begin{bmatrix} x_i^+ \\ d_i^+ \end{bmatrix} = \begin{bmatrix} A_i & 0 \\ 0 & I_p \end{bmatrix} \begin{bmatrix} x_i \\ d_i \end{bmatrix} + \begin{bmatrix} B_i \\ 0 \end{bmatrix} u$$
$$y_i = \begin{bmatrix} C_i & I_p \end{bmatrix} \begin{bmatrix} x_i \\ d_i \end{bmatrix}$$

8/23



Control structure equipped with one observer per each model:

$$\hat{x}_i(k+1) = A_i \hat{x}(k) + B_i u(k) \hat{d}_i(k+1) = \hat{d}_i(k) + L_i^d(C_i \hat{x}_i(k) - y(k) + \hat{d}_i(k))$$

• $\hat{d}(k)$ is an estimation of the output disturbance.

x(k) ∈ X, u(k) ∈ U, for all k ≥ 0. X is convex and closed,
 U is convex and compact and both sets contain the origin in their interior.

• A_i is stable. The pair (A_i, B_i) is controllable.

► f_{eco}(y, u, ρ) is a convex nonlinear function that takes into account the economic objectives of the plant.

$$\begin{array}{lll} (x_s^*, u_s^*, y_s^*) &=& \arg\min_{(x, u, y)} f_{eco}(y, u, \rho) \\ & s.t. \quad x \in \mathcal{X}, \quad u \in \mathcal{U} \\ & x = A_r x + B_r u, \quad y = C_r x \end{array}$$

ρ is a parameter that takes into account prices, costs or production goals.

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The stationary conditions of each model can be mapped in a *m*-dimensional linear subspace s. t.

$$(x_{s,i}, u_s) = M_{\theta,i}\theta, \quad y_{s,i} = N_{\theta,i}\theta$$

given a parameter $\theta \in \mathbb{R}^m$.

 The sets of admissible equilibrium states, inputs and outputs are

$$\mathcal{Z}_{s,i} = \{ (x_i, u) \in \mathcal{X} \times \mathcal{U} \mid x_i = A_i x_i + B_i u \}$$

$$\mathcal{X}_{s,i} = \{ x_i \in \mathcal{X} \mid \exists u \in \mathcal{U} \text{ such that } (x_i, u) \in \mathcal{Z}_{s,i} \}$$

$$\mathcal{Y}_{s,i} = \{ y = C_i x_i \mid (x_i, u) \in \mathcal{Z}_{s,i} \}$$

Multi-model one-layer MPC

Include the RTO economic objective in the MPC control problem.

- Economic and dynamic objectives in one optimization problem.
- Reduces incosistency/unreachability.
- Better economic performance.

The proposed cost function reads:

$$V_N(x, \hat{d}, \rho; \mathbf{u}, \theta) = \sum_{j=0}^{N-1} ||x_{no}(j) - x_{s, no}||_Q^2 + ||u(j) - u_s||_R^2 + V_O(h_s, u_s, \rho)$$

where

$$V_O(h_s, u_s, \rho) = \sum_{i=1}^{L} f_{eco}(y_{s,i}, u_s, \rho), \text{ and } h_s = \begin{bmatrix} y_{s,1} \\ \vdots \\ y_{s,L} \end{bmatrix}$$

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Optimization problem Problem $P_N(x, \hat{z}, \hat{d}, \rho, \tilde{u}, \tilde{\theta})$

$$\begin{array}{ll} \min_{\substack{\mathbf{u},\theta\\\mathbf{u},\theta}} & V_N(x,\hat{d},\rho;\mathbf{u},\theta) \\ s.t. & x_i(0) = \hat{x}_i, & i \in \mathbb{I}_{1:L} \\ & x_i(j+1) = A_i x_i(j) + B_i u(j), & j \in \mathbb{I}_{0:N-1}, & i \in \mathbb{I}_{1:L} \\ & x_i(j) \in \mathcal{X}, & u(j) \in \mathcal{U}, & j \in \mathbb{I}_{0:N-1}, & i \in \mathbb{I}_{1:L} \\ & (x_{s,i},u_s) = M_{\theta,i}\theta, & i \in \mathbb{I}_{1:L} \\ & y_{s,i} = N_{\theta,i}\theta + \hat{d}_i, & i \in \mathbb{I}_{1:L} \\ & x_i(N) = x_{s,i} & i \in \mathbb{I}_{1:L} \\ & V_N^i(\hat{x}_i, \hat{d}_i, \rho; \mathbf{u}, \theta) \leq V_N^i(\hat{x}_i, \hat{d}_i, \rho; \mathbf{\tilde{u}}, \tilde{\theta}), & i \in \mathbb{I}_{1:L} \end{array}$$

where

$$V_{N}^{i}(\hat{x}_{i},\hat{d}_{i},\rho;\mathbf{u},\theta) = \sum_{j=0}^{N-1} ||x_{i}(j)-x_{s,i}||_{Q}^{2} + ||u(j)-u_{s}||_{R}^{2} + f_{eco}(y_{s,i},u_{s},\rho)$$

- ► ũ and θ̃ are feasible solutions, based on a solution of the same problem at time k - 1.
- Last constraint: robust stability constraint (Badgwell, 1997).

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Theorem

For any ρ , the closed-loop system controlled by the proposed controller is stable and converges asymptotically to a steady point $(x_s^*, u_s^*, y_s^*) = \arg\min_{(x, u, y)} f_{eco}(y, u, \rho).$

Sketch of the proof:

• Recursive feasibility is ensured by the fact that the real plant $\pi_r \in \Pi$.

Cost decreasing is ensured by the robust constraint

 $V_{N}^{i}(\hat{x}_{i},\hat{d}_{i},\rho;\mathbf{u},\theta) \leq V_{N}^{i}(\hat{x}_{i},\hat{d}_{i},\rho;\tilde{\mathbf{u}},\tilde{\theta}), \ i \in \mathbb{I}_{1:L}$

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Properties of the proposed controller

- The controller ensures feasibility under any change of the economic objective.
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Simulation example

The 4 tanks plant

Interesting features:

- 1. All the states are measurable.
- 2. The outputs are strongly coupled.
- 3. The system is nonlinear.
- 4. The states and inputs are constrained.

$$\begin{aligned} \frac{dh_1}{dt} &= -\frac{a_1}{A}\sqrt{2gh_1} + \frac{a_3}{A}\sqrt{2gh_3} + \frac{\gamma_a}{A}\frac{q_a}{3600} \\ \frac{dh_2}{dt} &= -\frac{a_2}{A}\sqrt{2gh_2} + \frac{a_4}{A}\sqrt{2gh_4} + \frac{\gamma_b}{A}\frac{q_b}{3600} \\ \frac{dh_3}{dt} &= -\frac{a_3}{A}\sqrt{2gh_3} + \frac{(1-\gamma_b)}{A}\frac{q_b}{3600} \\ \frac{dh_4}{dt} &= -\frac{a_4}{A}\sqrt{2gh_4} + \frac{(1-\gamma_a)}{A}\frac{q_a}{3600} \end{aligned}$$



Simulation example

Linearized model:

$$\frac{dx}{dt} = \begin{bmatrix} \frac{-1}{\tau_1} & 0 & \frac{A}{A\tau_3} & 0\\ 0 & \frac{-1}{\tau_2} & 0 & \frac{A}{A\tau_4}\\ 0 & 0 & \frac{-1}{\tau_3} & 0\\ 0 & 0 & 0 & \frac{-1}{\tau_4} \end{bmatrix} x + \begin{bmatrix} \frac{\gamma_a}{3600A} & 0\\ 0 & \frac{\gamma_b}{3600A}\\ 0 & \frac{(1-\gamma_b)}{3600A} & 0 \end{bmatrix} u$$

where
$$x_i = h_i - h_i^o$$
, $u_j = q_j - q_j^o$, $j = a, b$ and $i = 1, \dots, 4$.
 $\tau_i = \frac{A}{a_i} \sqrt{\frac{2h_i^0}{g}} \ge 0, i = 1, \dots, 4$.

Models:linearization points

Model	h_1	h ₂	q a	q_b
π_1	0.4210	0.4678	1.4802	1.5197
π_2	0.2977	0.3308	1.2447	1.2779
π_3	0.8550	0.5672	1.0444	2.6980
π_{no}	0.6487	0.6636	1.63	2

- Model π_{no} is the nominal model.
- Model π_1 is been taken as the real plant model.

Simulation example

Economic cost function:

$$f_{eco}(y, u, \rho) = (q_a^2 + \rho_1 q_b^2) + \rho_2 \frac{V_{min}}{A(h_1 + h_2)}$$

where $y = (h_1, h_2)$, $u = (q_a, q_b)$, $\rho = (\rho_1, \rho_2)$, and V_{min} is the minimum volume to be accumulated.

•
$$\rho^{[1]} = (1, 20), \, \rho^{[2]} = (1, 10) \text{ and } \rho^{[3]} = (0.4, 30).$$

• MPC setup: $Q = I_4$, $R = 0.01 I_2$, and N = 6.

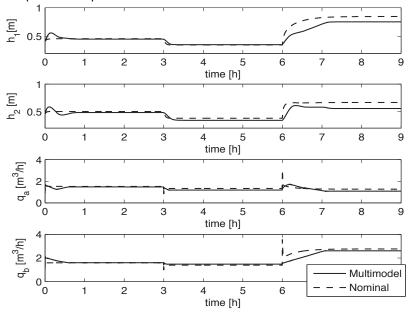
Constraints:

$$\begin{array}{rrrr} 0.2 & \leq h_i \leq & 1.20 \, [m] \\ 0 & \leq q_a \leq & 3.26 \, [m^3/h] \\ 0 & \leq q_b \leq & 4.00 \, [m^3/h] \end{array}$$

Simulations in Matlab using *fmincon*.

Simulation results

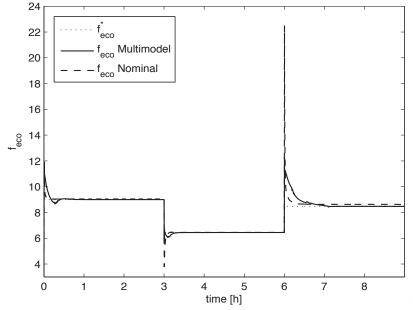
Outputs and inputs: time evolutions



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Simulation results

Economic costs: time evolutions



20/23

Summary

Conclusions:

- A multi-model one layer RTO+MPC strategy has been proposed to reduce inconsistencies in the traditional hierarchical structure RTO/MPC.
- The multi-model approach ensures robustness to model uncertainties or changes in the operative conditions.
- Recursive feasibility and convergence are always ensured, for any changing economic objective.
- Stability is proved resorting to Lyapunov arguments.

Future works:

Nonconvex f_{eco}.

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Thanks for your attention!

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